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ABSTRACT

Despite the intense concentration on lithium-based batteries, safety, ease of construction and cost continue to drive the search for alternatives that do not suffer from such restrictions. We present here preliminary work on the development of thin film Mg^{2+} conducting electrolytes as the key starting point for the development of all-solid-state Mg batteries. Initial studies explored compositions in the Mg_{0.5}Ce_xZr_{2-x}(PO₄)₃ (x = 0.1, 0.2 and 0.3) system first as pellets and with somewhat optimized compositions (with x = 0.2) as thin films. Introduction of Ce allows sintering to full density at temperatures where Ce free films do not densify completely. The work reported here relies on the synthesis of nanopowders (NPs) using liquid-feed flame spray pyrolysis that offers the potential to reduce processing conditions, to control final average grain sizes (AGSs) and provide single-phase materials with good to excellent mechanical properties. The pellets and then thin (\leq 50 µm) films produced here show conductivities of up to 3×10^{-3} mS cm⁻¹ at ≈ 300 °C, which if extrapolated (using an E_a of ≈ 30) to 400 °C would be close to 10^{-2} mS cm⁻¹ in keeping with the best reported values in the literature. The thin films reported here offer nearly full densities beyond what is currently achievable by any other method. The ionic area specific resistance (IASR) values for these thin films were found to be 1400 Ω cm² at 300 °C and are estimated to drop to $110\,\Omega\,cm^2$ at 400 °C, significantly lower than values for pellets reported elsewhere.

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1. Introduction

Electrical energy storage demands of electric devices (including electric vehicles, laptop computers, load leveling for stationary power sources and cellular phones for example), coupled with fossil fuel economies and limitations demonstrate the growing need for rechargeable batteries with multiple performance capabilities including sufficient energy density, appropriate voltage and current capabilities, and perhaps most important very low safety requirements. Conventional liquid electrolytes lithium batteries suffer from the potential to fail catastrophically via electrolyte

* Corresponding author. E-mail address: talsdad@umich.edu (R.M. Laine). stances, all-solid-state batteries (ASBs) have been proposed as a fundamental solution [4]. They do not require liquid electrolytes relieving this avenue for catastrophic failure. They are also capable of operating over wide temperature and electrochemical potential ranges. Coincidently, metal anodes and high-voltage cathodes can be used to greatly enhance energy densities allowing long term operation without need to recharge. Likewise, the potential for much greater operating temperature ranges implies faster charge/ discharge properties.

To date, the most successful and widely implemented rechargeable battery technologies rely on lithium. Efforts to

leakage, boiling, freezing, combustion or even explosion, of particular importance for in vivo applications [1-3]. There is need

to develop batteries with much higher safety and greater energy

densities to satisfy growing market demands. Under such circum-

https://doi.org/10.1016/j.electacta.2018.04.015 0013-4686/© 2018 Elsevier Ltd. All rights reserved. develop rechargeable Li ASBs have attracted much attention due to their high voltage and high theoretical energy density of $3500 \text{ Wh} \cdot \text{kg}^{-1}$, and can, when perfected, play a pivotal role as an advanced electrochemical power source [3,5,6]. However, the low accessibility of Li (e.g. low natural abundance of 7 g/F in the earth's crust and 0.04–1.16% in brine ponds) goes against its sustainability. High and probably rising costs also limit the future use of Li⁺ batteries for large-scale applications [6–8].

Given the need for a sustainable supply of large-scale energy storage devices, considerable efforts have been directed towards the development of non-lithium battery systems, especially ASBs. Of the possible alternatives, rechargeable magnesium-ion (Mg^{2+}) battery technology offers significant opportunities for the following reasons. First is Mg's high natural abundance in the earth's crust (5th most abundant element, approximately 10⁴ times that of Li), allowing low-cost incorporation into battery elements. Second, the divalent nature of Mg ions also allows a high volumetric capacity of 3833 mAh/cc (vs. 2046 mAh/cc for lithium). Third, Mg provides a higher atmospheric stability and melting point than Li making it safer compared to Li. Mg also has a rather low equivalent weight of 12 g per Faraday (F) (vs. 7 g/F for Li, 23 g/F for Na) and low price of ca \$2700/ton (currently ca. 24 times cheaper than Li) ensuring a feasible, "environmentally-friendly" alternative to the immensely popular Li-ion systems [6,8-21].

To date, there have been a number of reviews [7-10] discussing the potential offered by Mg based batteries. Much of the literature on Mg based batteries that function near ambient focuses on the use of liquid electrolytes [18-21]. Thus, the same issues of safety would apply for any system that was commercialized. Despite the exceptional interest in making solid state Mg electrolytes [1,7-9,15-17,22], only one recent theoretical paper suggests that it should be possible to make solid state electrolytes with near ambient conductivities sufficient to be used to generate solid state Mg based batteries [14]. Thus, at present Mg based solid state batteries seem to offer potential only for high temperature applications.

Despite these positive attributes, the development of Mg-based ASBs has not kept pace with Li batteries. One critical issue impeding progress is the availability of stable and highly Mg²⁺-conducting solid electrolytes that enable reversible release of Mg^{2+} ions from a magnesium metal anode. To date, there exist only limited reports on Mg²⁺-conducting solid electrolytes. Mg_{0.5}Zr₂(PO₄)₃, MZP, is well-known among them to have a 3-D network linking ZrO₆ octahedra and PO₄ tetrahedra by corner-sharing [18–21]. MZP has two crystal morphologies. The β -Fe₂(SO₄)₃-type MZP (monoclinic symmetry, P2₁/n space group) would offer reduced conductivities at low temperatures due to the distortion of the β -Fe₂(SO₄)₃ structure. MZP can also offer a NASICON (Na⁺ super ionic conductor) structure (rhombohedral symmetry with hexagonal setting, R3c) where well-ordered Zr₂P₃O₁₂ (lantern) units allow smooth ion migration. Therefore, high ion conductivity is expected at moderate temperatures (300°-500 °C) due to the low activation energy for ion migration.

Of the available reports on MZP systems, pellet-shaped electrolytes have been explored by a number of groups synthesized mainly using solid-state synthetic [21–24] and sol-gel methods [15–17]. Ikeda et al. [21,22,26] first investigated solid MZP electrolytes to develop potentiometric sensors. As-processed MZP pellets exhibited the expected Na_{0.5}Zr₂(PO₄)₃ structure with conductivities ranging from 2.9×10^{-2} mS cm⁻¹ (400 °C) to 6.1 mS cm⁻¹ (800 °C) and activation energies of ≈80 kJ/mol [21].

Imanaka et al. [23] also prepared MZP pellets by solid state processing finding Mg^{2+} conductivities were considerably enhanced predominantly due to the microscopic dispersion of a $Zr_2O(PO_4)_2$ secondary phase in the composite. Additionally, Anuar

et al. [15,16] prepared MZP pellets with a pure NASICON-phase by sol-gel processing observing conductivities of 1.0×10^{-3} mS cm⁻¹ at ambient and 7.1×10^{-2} mS cm⁻¹ at 500 °C with electrochemical stabilities up to 2.50 V vs a Mg/Mg²⁺ electrode. Adamu et al. [17] reported a conductivity of 6.9 mS cm⁻¹ at 800 °C for dense (ca. 99 % TD), single-phase MZP pellets produced using a novel sol-gel approach.

Efforts to improve the performance of MZP compounds have targeted modification of the lattice structures [16,27–29]. Thus substitution of Fe³⁺ (0.65 Å ionic radius) for Zr⁴⁺ (0.72 Å) is expected to reduce lattice dimensions providing more suitable channel sizes for Mg²⁺ (0.72 Å) migration. It also introduces extra interstitial Mg²⁺ ions in the NASICON structure anticipated to enhance the concentration of available Mg²⁺ ions [28]. Thus, introduction of Fe³⁺ increases charge carrier concentrations and mobile ion concentrations. The partially Fe-substituted MZP, i.e. Mg_{0.9}(Zr_{0.6}Fe_{0.4})₂(PO₄)₃ gives a maximum conductivity of 1.3×10^{-2} mS cm⁻¹ at room temperature and 7.2×10^{-2} mS cm⁻¹ at 500 °C, an order of magnitude higher than that of the parent MZP compound [16].

The thicknesses (1–2 mm) of pellet components including electrodes and electrolytes limit gravimetric/volumetric energy densities of assembled cells. Thicker components with relatively higher internal resistance cause lower power output (poor rate capability) and an earlier stop of discharge (particularly high rate discharge) due to longer diffusion distances and severe concentration polarization [30–33]. Compared to pellets, thin (\leq 100 µm) film electrolytes are therefore more competitive and useful in assembling cells with high packing densities and structural stability ensuring high safety and overall performance of assembled battery systems [34–43]. One can envision developing solid-state batteries with superior energy densities through significant reductions in the electrolytes and electrode thicknesses opening a new door for Mg batteries.

We recently described methods of processing dense Li_{1.7}Al_{0.3-} Ti_{1.7}Si_{0.4}P_{2.6}O₁₂ pellets with ambient ionic conductivities >1 mS cm⁻¹ [37]. Significantly, we also learned to process dense, flexible Li⁺-conducting ceramic electrolyte thin films (\leq 50 µm) using tape-casting methods based on liquid-feed flame spray pyrolysis (LF-FSP) nanopowders (NPs). These systems provide high ambient ionic conductivities (e.g. 0.4 mS cm⁻¹ for 50 µm Li_{1.7}Al_{0.3-}Ti_{1.7}Si_{0.4}P_{2.6}O₁₂ [37], 0.2 mS cm⁻¹ for 30 µm c-Li₇La₃Zr₂O₁₂ [38], 1.3 mS cm⁻¹ for 25 µm Ga:LLZO [39]) and high tolerance to heat improving safety over wide operating temperatures.

In this contribution, we extend our efforts to develop Ce-doped MZP thin film electrolytes with chemical compositions near $Mg_{0.5}Ce_xZr_{2-x}(PO_4)_3$ (x = 0.1, 0.2 and 0.3), hereinafter referred to as MZPCe_x. Ce⁴⁺ (0.87 Å) is expected to substitute for Zr⁴⁺ (0.72 Å) as an alternative to Fe³⁺ to improve MZP conductivities. MZPCe_x pellets ($\Phi 12 \times 0.5 \text{ mm}^2$) were first studied to optimize compositions, and then thin ($\leq 50 \mu$ m) films were processed with these somewhat optimized compositions. Pellets and thin films with compositions of $Mg_{0.5}Ce_{0.2}Zr_{1.8}(PO_4)_3$ offer ionic conductivities in keeping with the best reported values in the literature [15,17,20,23].

2. Experimental

2.1. Raw materials

Magnesium hydroxide $[Mg(OH)_2]$, propionic acid (CH₃CH₂COOH), isobutyric acid $[(CH_3)_2CHCO_2H]$, isobutyric anhydride $[(C_3H_7CO)_2O]$, zirconium basic carbonate, $[Zr(OH)_2CO_3 \cdot ZrO_2]$, triethyl phosphate $[(C_2H_5O)_3PO]$, cerium carbonate $[Ce_2(CO_3)_3 \cdot xH_2O]$, methyl ethyl ketone $(C_2H_5COCH_3)$ and benzyl butylphthalate $\{2-[CH_3(CH_2)_3O_2C]C_6H_4CO_2CH_2C_6H_5, 98\%\}$ were

purchased from Sigma-Aldrich (Milwaukee, WI). Polyvinyl butyral $[(C_8H_{14}O_2)_n, B-98, M_n = 40,000-70,000]$ was purchased from Butvar (Avon, OH), and absolute ethanol from Decon Labs (King of Prussia, PA).

2.2. Precursor synthesis

As-purchased triethyl phosphate, $(C_2H_5)_3PO_4$, was directly used as the P source. The other three precursors were synthesized as sources of Mg, Zr, and Ce, respectively as follows.

Magnesium propionate, $Mg(O_2CCH_2CH_3)_2$, was synthesized by reacting $Mg(OH)_2$ (157 g, 2.7 mol) with excess $CH_3CH_2CO_2H$ (500 ml, 6.8 mol) in a 1 L round-bottom flask equipped with a still head. The mixture was heated at 130 °C for 2 h with magnetic stirring until it became transparent. On cooling to room temperature, magnesium propionate crystallized, then was filtered off, dried naturally, ground into powder for use. As-obtained Mg precursor provided a ceramic yield of ca. 42 wt %, lower than theoretical value (44 wt %), as determined by TGA. The discrepancy arises mainly from slight excess of propionic acid.

Zirconium isobutyrate, $Zr[O_2CCH(CH_3)_2]_2(OH)_2$, was synthesized by reacting zirconium basic carbonate (160 g, 0.52 mol) with isobutyric acid (390 g, 4.4 mol) and isobutyric anhydride (350 g, 2.2 mol) in a 1 L flask equipped with a still head in N₂ atmosphere. The reactants were heated at 110 °C until they became transparent. Zirconium isobutyrate crystallized on cooling, then was filtered off, dried, ground into powder for use.

Cerium propionate [Ce(O₂CCH₂CH₃)₃(OH)] was synthesized by reacting cerium carbonate (46 g, 0.1 mol) with excess propionic acid (225 mL, 3 mol) and propionic anhydride (65 mL, 0.5 mol) in a 1 L flask equipped with a still head. The solution was heated at 120 °C for 10 h with magnetic stirring until a transparent dark orange liquid was obtained. On cooling to room temperature, cerium propionate crystallized and was filtered out.

2.3. Nanopowder (NP) syntheses

 $Mg_{0.5}Ce_xZr_{2-x}(PO_4)_3$ (x = 0.1, 0.2 and 0.3) NPs were synthesized by liquid feed-flame spray pyrolysis (LF-FSP) technology described in detail elsewhere [40–43]. All the precursors for Mg, Zr, P, Ce were mixed and dissolved in ethanol at designated ratios providing a solution with 3 wt % ceramic yield. The as-formulated precursor solution was aerosolized with oxygen into a 1.5 m long combustion chamber and ignited using methane/O₂ pilot torches. After combustion and cooling, NPs were collected downstream in wire-intube electrostatic precipitators operated at 10 kV, then cleaned by dispersing them into EtOH using an ultrasonic horn (Vibra-cell VC-505, Sonics & Mater. Inc.). After sufficient sedimentation, the supernatant suspension was decanted into a container, dried in an oven and collected for use.

2.4. Pellet processing

The dried MZPCe_x powders were sieved through a 20 μ m polymer mesh, uniaxially pressed at 12 MPa in a biaxial-compression WC die (14.2 mm in diam.), and CIPped at 200 MPa for 30 min improving densities of green bodies. Green pellets were sintered in air at 1100–1200 °C for 1 h with a ramp rate of 5 °C/min.

2.5. Thin film processing

As-synthesized MZPCe_{0.2} NPs were mixed with binder, plasticizer and solvents with designated ratios (as listed in Table 1), then ball-milled for 24 h with zirconia beads (99% in purity, 3.0 mm in diam.) homogenizing the suspension.

Table 1

Starting chemical	components	for	film	casting.
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Components	Roles	Mass (g)	Wt.%	Vol%
MZPCe _{0.2}	Powder	1.00	32	10
Polyvinyl butyral (PVB)	Binder	0.13	4	4
Benzyl butyl phthalate (BBP)	Plasticizer	0.13	4	4
Methyl ethyl ketone (MEK)	Solvent	0.95	30	41
Ethanol	Solvent	0.95	30	41

The suspension was cast using a wire-wound rod coater (Automatic Film Applicator-1137, Sheen Instrument, Ltd., UK) producing thin NP filled polymeric films. Film thicknesses were controlled using spacers between the rod and Mylar substrate. After solvent evaporation, dried green films were cut into small pieces, uniaxially pressed at 30 MPa/100 °C/3 min using a heated bench-top press (Carver, Inc), then manually peeled off the substrate.

Dried, green MZPCe_{0.2} films were debindered/crystallized in air at 785 °C/1 h heating at a ramp rate of 5 °C/min followed by sintering at 1000–1200 °C for selected dwell times. During heating, films were placed between α -alumina plates to prevent warping.

2.6. Thermal etching of as-sintered films

To calculate average grain sizes using the lineal intercept method, as-sintered films were thermally etched to expose separate grains by heating in air for 30 min at designated temperatures for 30 min in air. The temperatures of thermal etching were usually 100 °C lower than sintering temperatures of films.

2.7. Characterization

Specific surface area (SSA) analyses of the as-shot MZPCe_{0.2} NPs were obtained using a Micromeritics ASAP 2010 N₂ adsorption analyzer (Norcross, GA). Samples (ca. 200 mg) were degassed at 400 °C until the degas rate was less than 0.005 Torr/min, then analyzed at -196 °C (77 K) in N₂. SSAs were calculated using the BET multipoint (\geq 10 points) method within the relative pressure range of 0.001–0.20. Additionally, the average particle sizes (APSs), *D*, can be calculated per formula [44]:

$D = 2r = 6/(\rho \times SSA)$

where ρ is the theoretical density of powders, and r is the particle radius.

2.7.1. Thermogravimetric/differential scanning calorimetry (TG/ DTA)

Thermal decomposition and crystallization of as-cast green films were analyzed using Q600 simultaneous TG/DTA (TA Instruments, Inc.) predicting the progress of film thermal behavior. Samples (ca. 15 mg) were loaded in an alumina pan, heated from ambient temperature to 1200 °C with a ramp rate of 10 °C/min in a flowing synthetic air (60 mL/min).

X-ray diffraction (XRD) (Rigaku Denki., LTD., Tokyo, Japan) was conducted at 40 kV and 100 mA for phase identification of LF-FSP NPs and sintered films and pellets. Note that the pellets were broken up, ground into powders and then characterized by XRD. Samples were scanned by Cu K α radiation ($\lambda = 1.541$ Å) at 2°/min within the range of 10–70° 2 θ with 0.02° intervals. Jade 2010 software (Version 1.1.5 from Mater. Data, Inc.) was used to analyze XRD data where JCPDS files were used including Mg_{0.5}Zr₂(PO₄)₃ (04-016-0487), ZrP₂O₇ (04-009-9317) and ZrO₂ (98-000-9216). The Jade software (2010, Version 1.1.5 from Materials Data, Inc.,

Livermore CA) was used to refine lattice constants, and to determine the presence of crystallographic phases calculating their relative contents.

Scanning electron microscopy (SEM) (NOVA Nanolab, FEI Inc.) was run at 20 kV and used to observe powder and film morphologies. All the samples were sputter coated with a gold film using a Technics Hummer VI sputtering system (Anatech Ltd., Alexandria, VA) to improve resolution.

Transmission Electron Microscopy (TEM) (JEOL 3011) was conducted at 300 kV to study film microstructures including grain sizes and phases. As-sintered 40 μ m thick films were cut to 3 mm in diam., gently polished, dimpled, and Ar-ion thinned to perforation.

lonic conductivity measurements were run using an AC broadband dielectric impedance spectrometer (Novocontrol technologies, Hundsangen, Germany) to evaluate the ionic conductivity of as-sintered MZPCe_{0.2} films. All film surfaces were gently polished using 1200 grit SiC sandpapers (LECO, St. Joseph, MI), then coated with gold coatings using an SPI sputter coater (SPI Supplies Inc., West Chester, PA). Gold electrode with a diam. of 1 mm was deposited on one side of film surface, while the other side was coated in full. Ionic conductivity measurements were operated at 60–280 °C with a frequency range of 10 MHZ to 0.1 HZ and a root mean square (RMS) voltage of 10 mV.

Nyquist plots were fitted using EIS spectrum analyzer software to get total resistance of samples [45]. Conductivities (σ_t) were calculated from formula [46,47].

$$\sigma_t = d/(A_e \times R) \tag{1}$$

where d, A_e , R denote film thickness, electrode area and total resistance, respectively.

Activation energies, *E_a*, were calculated from Arrhenius equation [15,48].

$$\sigma_t = A \exp(-E_a/R_g T) \tag{2}$$

where A, R_g , T mean pre-exponential factor, gas constant and absolute temperature, respectively.

3. Results and discussion

3.1. As-produced NPs

As seen in Fig. 1a SEM, as-produced MZPCe_{0.2} NPs typical of MZP_x (x = 0.1, 0.2 and 0.3) consist of spherical agglomerated particles with few obvious aggregates. Most of the powders exhibit

average particle sizes (APSs) < 100 nm with no micron sized particles. BET studies indicate SSAs of $28 \text{ m}^2/\text{g}$ allowing calculation of APSs of ca. 66 nm, in accord with SEM results.

Fig. 1b XRD indicates these NPs consist primarily of MZP (74 wt %) with the remaining phases being ZrP_2O_7 (9 wt %) and ZrO_2 (17 wt %). The broad XRD peaks are typical of nanoscale particles. It should be noted that the presence of some partially amorphous powders cannot be excluded.

3.2. Thermal analysis of green films

As-cast green films were heated to 1200 °C/air with a ramp rate of 10 °C/min as a prelude to extensive further studies on sintering films and pellets. Thermal analysis (Fig. S1) shows continuous, significant mass losses (until around 550 °C) accompanied by exotherms arising at 320° and 500 °C, due mainly to decomposition of polymer additives, see Table 1. Mass losses cease at 550–600 °C corresponding to a ceramic yield of 79 wt % almost identical to theory derived from Table 1. The expected ceramic yields of processed green films can be calculated as 80 wt % (56 vol %), excluding solvents (MEK and ethanol) as they would evaporate on drying. The exotherm at 783 °C is likely associated with the crystallization of MZP and ZrP₂O₇ phases [15]. The endotherm seen above 1120 °C, accompanied by a slight mass loss, is most likely due to the evaporation of PO_x species [17,23].

3.3. *MZPCe_x* pellets

Fig. 2 provides XRDs for MZPCe_x (x = 0.1, 0.2 and 0.3) pellets after sintering at 1200 °C/1 h/air. The as-sintered pellets consist mainly of Mg_{0.5}Zr₂(PO₄)₃ and ZrP₂O₇ phases. As reported elsewhere, zirconium phosphate including Zr₂P₂O₉ and ZrP₂O₇ are typical impurities detected in MZP materials [17,25]. MZPCe_{0.1} pellets offer ca. 97 wt % MZP, while for most MZPCe_{0.2} and MZPCe_{0.3} pellets phase purity is closer to 90 wt % (Table 2).

Fig. 3 SEMs indicate that sintering MZPCe_x at 1200 °C/1 h/air offers almost fully dense MZPCe_{0.2} and MZPCe_{0.3} pellets, but porous MZPCe_{0.1} pellets with a relative density of \approx 90% (Table 2).

Note that the MZPCe_{0.2} pellets were also sintered at $1100 \circ C/1$ h, $1200 \circ C/3$ h, respectively. Unfortunately, lower temperatures lead to porous structures, and longer dwell times at $1200 \circ C$ lead to lower MZP phase contents. Higher temperatures and longer dwell times probably cause PO_x loss (SEM and EDS not shown), which leads to lower phase purities. *Ce-free MZP samples do not densify on sintering at 1000–1200* °C under the same conditions (SEM not shown).



Fig. 1. (a) SEM image and (b) XRD pattern of as-produced MZPCe_{0.2} powders. Note that cracked coating on particle surfaces are sputtered gold added to aid imaging.



Fig. 2. XRD patterns of MZPCe_x pellets after sintering at $1200 \circ C/1$ h/air.

Optimization of the initial chemical compositions to ensure producing high-purity MZP NPs would be one possible set of studies for future work. Sintering conditions must also be further optimized to produce still higher purity pellet electrolytes.

Lower relative densities and phase purities would lead to lower ionic conductivities of Ce-free MZP, MZPCe_{0.1} and MZPCe_{0.3} pellets. Therefore, only the ionic conductivities of fully dense MZPCe_{0.2} pellets with relative densities of at least 90% were investigated. Fig. 4 provides Nyquist plots in the high frequency regions for MZPCe_{0.2} pellets tested at 100° and 200 °C, respectively. At 100 °C, the Nyquist plot shows a nearly perfect semicircle (<18 M Ω in impedance). An imperfect semicircle at higher frequencies (<0.5 M Ω in impedance) followed by an inclined spike at lower frequencies (>0.5 M Ω in impedance) is observed at 200° vs. 100 °C.

Both plots are typical of ionic conductors with blocking electrodes. The semicircle and spike are due to samples' ionic conductivity and polarization of ion-blocking electrodes [48]. In this study, since the left intercept of the semicircle with the real axis (Z') approaches zero, the right intercept is taken as the total resistance ($R_t = R_g + R_{gb}$) as a conservative estimate: R_g and R_{gb} denote the grain and grain boundary resistances, respectively [37–39]. A well-recognized equivalent circuit, as presented in the inset in Fig. 4a, is used for fitting providing the total resistance. The single resistor (R_1) is equal to the left intercept, the parallel resistor (R_2) to a constant phase element (CPE_1) is equal to the diameter of semicircle, and a constant phase element (CPE_2) denotes electrode polarization [48–51].

Table 3 lists the ionic conductivities of MZPCe_{0.2} pellets tested at $25-200 \,^{\circ}$ C. They offer ionic conductivities of $2.6 \times 10^{-6} \, \text{mS cm}^{-1}$ atambienttemperature, $>10^{-5} \, \text{mS cm}^{-1}$ at $100 \,^{\circ}$ C,and $3.8 \times 10^{-4} \, \text{mS cm}^{-1}$ at $200 \,^{\circ}$ C. Relevant discussion is presented inthe last section.

3.4. MZPCe_{0.2} films

3.4.1. Sintered film analyses

Per the investigation of MZPCe_x pellet sintering, MZPCe_{0.2} films were sintered at 1000–1200 $^{\circ}$ C aiming to obtain dense, phase-pure films at temperatures as low as possible.

Fig. 5 XRD patterns reveal phase compositions of the as-sintered MZPCe_{0.2} films. MZP forms in sintered films as well as ZrP_2O_7 as a minor secondary phase. Increasing sintering temperatures and dwell times leads to increases in Mg_{0.5}Zr₂(PO₄)₃, and decreases ZrP₂O₇ contents as show in Table 4. High-purity MZPCe_{0.2} films containing >99 wt % MZP were obtained on sintering at 1200 °C/ 3 h.

Fig. 6 SEMs show fracture morphologies for as-sintered MZPCe_{0.2} films. At 1000 °C, closed-packed spherical NPs are still observed, somewhat similar to as-produced NPs. At 1100 °C, these spherical morphologies disappear accompanied by formation of irregularly-shaped grains. Coincidentally, a large number of pores are distributed uniformly in films. At 1200 °C/1 h, almost no pores can be observed suggesting nearly fully dense films. Longer dwell times (3 h) lead to higher densification and somewhat larger grains. Calculation per Archimedes' method indicates relative densities of 95 \pm 2%. The fully dense films (50 µm thick) fracture in an intra-

Table 2

Densities and phase compositions of MZPCex pellets after sintering at 1200 °C/1 h/air.

-		• • •		
Materials	Density (g cm ⁻³)	Relative density (%)	Phases	
			MZP (wt. %)	ZrP ₂ O ₇ (wt. %)
MZPCe _{0.1}	2.95	90(±2)	97	3
MZPCe _{0.2}	3.32	100(-2)	90	10
MZPCe _{0.3}	3.41	100(-2)	87	13



Fig. 3. SEMs of fresh fracture surfaces of (a) MZPCe_{0.1}, (b) MZPCe_{0.2} and (c) MZPCe_{0.3} pellets after sintering at 1200 °C/1 h/air.



Fig. 4. Representative Nyquist plots for MZPCe_{0.2} pellets tested at (a) 100 °C and (b) 200 °C. The top right insert in (a) is the equivalent circuit used for fitting. R and CPE denote resistors and constant phase elements, respectively.

Table 3 lonic conductivities of MZPCe_{0.2} pellets after sintering at 1200 $^\circ\text{C}/1$ h/air.

<i>T</i> (C)	25	40	60	80	100	120	140	160	180	200
σ_t ($ imes 10^{-5}\mathrm{mScm^{-1}}$)	0.26	0.53	0.63	0.79	1.2	1.9	3.8	8.4	19	38



Fig. 5. XRD patterns of MZPCe_{0.2} films after sintering at 1000–1200 °C in air.

Table 4

Relative contents	s of phases	in sintered	MZPCe _{0.2} films.
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Temperature (°C)/Time (h)	MZP (wt. %)	ZrP ₂ O ₇ (wt. %)
1000/1	91.8	8.2
1100/1	93.7	6.3
1200/1	96.1	3.9
1200/3	>99.0	<1.0

granular mode and show a flat fracture surface. Additionally, the white, plate-like grains in Fig. 6c–d correspond to the secondary ZrP_2O_7 phase, as confirmed by TEM, see below.

Initial efforts were made to calculate average grains sizes (AGSs) by observing surface and fracture morphologies of thermally

etched MZPCe_{0.2} films using SEM. Both the surfaces and fractured surfaces of the as-sintered films at 1200 °C/3 h were thermally etched at 1100 \pm 100 °C/30 min in air. However, only ambiguous grain boundaries or separated grains were observed (SEMs not shown). TEM was then used to investigate AGSs (Fig. S2). Fig. S2a provides a representative TEM of the as-sintered MZPCe_{0.2}films at 1200 °C/3 h in air. Grains with clear boundaries were observed. Statistical calculation of dozens of grains based on the lineal intercept method indicates AGSs of 550 \pm 100 nm in 45 \pm 5 μ m thick films. Fig. S2b shows a representative TEM image indicating presence of secondary ZrP₂O₇ phases with AGSs of ca. 200 nm, which is consistent well with the observation of morphologies using SEM (Fig. 6).

Different sintering conditions result in diverse microstructures with variations in phase compositions, grain sizes, phase segregation at grain boundaries and relative densities thereby influencing significantly the ionic conductivity of electrolytes. Low relative densities of electrolytes and purities of the main phase lead to high values for grain boundary resistance [52,53]. A single-phase microstructure with full density and small grain sizes is thus an essential prerequisite for high-performance ionic conductors. Therefore, the ionic conductivities of fully dense MZPCe_{0,2} films with high phase purities (>99%) were investigated as discussed below.

3.4.2. Ionic conductivities

In this work, six MZPCe_{0.2} films sintered at 1200 °C/3 h in air were used to measure ionic conductivities. Conservative results with reproducibility were adopted. Fig. 7 depicts representative Nyquist plots for MZPCe_{0.2} films tested at 100° and 200 °C, respectively. Depressed semicircles at higher frequencies were observed followed by inclined spikes at lower frequencies. The equivalent circuit presented in Fig. 7a inset, as noted in section 3.3, was used for fitting to get the total resistance. The calculated ionic conductivities of MZPCe_{0.2} films measured at 25–280 °C are listed in Table 5. MZPCe_{0.2} films provide conductivities of 1.3 × 10⁻⁶ mS cm⁻¹ at 60 °C, increasing to 10⁻⁴ mS cm⁻¹ at 200 °C and of 3.1 × 10⁻³ mS cm⁻¹ at 280 °C.



Fig. 6. SEMs of fractured MZPCe_{0.2} films after sintering in air at (a) 1000 °C/1 h, (b) 1100 °C/1 h, (c) 1200 °C/1 h and (d) 1200 °C/3 h.



Fig. 7. Representative Nyquist plots for MZPCe_{0.2} film samples tested at (a) 100 °C and (b) 200 °C. The lower right insert in (a) is the equivalent circuit used for fitting, the same as that for pellets in Fig. 5.

Table 5

Total conductivities (σ_t) of MZPCe_{0.2}films (43 ± 2 µm thick).

<i>T</i> (°C)	25	40	60	80	100	120	140	160	200	240	280
$\sigma_t (\times 10^{-5}{ m mScm^{-1}})$	0.02	0.05	0.13	0.23	0.43	0.81	1.4	3.5	19	91	310

The calculated activation energy is 29.6 kJ/mol (\geq 60 °C) derived from the slope of Arrhenius plot shown in Fig. 8. Lower activation

energies lead theoretically to higher conductivities, while higher activation energies lead to reduced conductivities at lower



Fig. 8. Arrhenius plot for MZPCe_{0.2} films based on Table 5 data.

Table 6

Estimated conductivities (σ_t) of MZPCe_{0.2} films based on Fig. 8 Arrhenius plot using the extension method.

T (°C)	400	500	600	700	800
$\sigma_t(\times 10^{-2}\mathrm{mScm^{-1}})$	4	19	63	166	365

temperatures. As reported elsewhere, $(Mg_{0.1}Hf_{0.9})_{4/3.8}Nb(PO_4)_3$ pellet electrolytes have activation energies of 64 kJ/mol coincident with ionic conductivities of $2.1 \times 10^{-3} \text{ mS cm}^{-1}$ at 300 °C [18], 20 times higher than that $(1.1 \times 10^{-4} \text{ mS cm}^{-1})$ of $Mg_{0.7}(Zr_{0.85}Nb_{0.15})_4P_6O_{24}$ pellets with higher activation energies of 92 kJ/mol [54].

Per Fig. 8 Arrhenius plot, ionic conductivities of MZPCe_{0.2} films at higher temperatures were estimated by extrapolation, and listed in Table 6. Table 7 compares the ionic conductivities of MZPCe_{0.2} films and pellets to other MZP counterparts reported elsewhere. MZPCe_{0.2} pellets offer conductivities of 3.8×10^{-4} mS cm⁻¹ at 20 °C, twice as high as the MZPCe_{0.2} films. The films have relative

Table 7

Found and estimated	I [†] MZP electrolyte	conductivities (σ_t)) reported here	and elsewhere.
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densities of 95% almost as high as that (98%) of pellets, and phase purities of 99% higher than that (90%) of pellets. The pellet surfaces were polished to obtain a mirror finish before measurement of conductivities. However, the thin films could not be polished easily because they are quite fragile compared to pellets. The low smoothness and even possible surface impurities are likely reasons for the lower conductivities of films vs pellets. The reasonably small AGSs ($550 \pm 100 \text{ nm}$) of MZPCe_{0.2} films may also lead to lower conductivities.

The MZPCe_{0.2} pellets and thin (\leq 50 µm) films show conductivities of up to 3 × 10⁻³ mS/cm² at approximately 300 °C in keeping with reported values in the literature. Note that conductivities reported in the open literature to date are only for MZP electrolyte pellets, whereas the present report is the first to produce thin films. Coincidently, films provide lower ionic area specific resistances (IASR = d/σ) due to the significant reduction in thicknesses [35,55–57].

The calculated *IASR* for 43 μ m *MZPCe*_{0.2} films was 1400 Ω cm² at \approx 300 °C. If we use an E_a of \approx 30 kJ/mol then we can extrapolate to suggest that *IASR* values for 43 μ m *MZPCe*_{0.2} films would be 110 Ω cm² at 400 °C. They are 20⁺ times smaller than values for 1 mm pellets with almost the same conductivities reported elsewhere [12,15,18–20]. However, this type of extrapolation can only be verified by actual temperature measurements which are beyond the capability of our current system.

Optimization of Ce-doped MZP NP synthesis, film processing and sintering leading to values of conductivities beyond those reported in open literature remains to be done in future work. MZP electrolytes with new substitutional dopants, e.g. Y^{3+} , are under exploration.

4. Conclusions

 $Mg_{0.5}Ce_xZr_{2-x}(PO_4)_3~(x=0.1,~0.2~and~0.3)$ electrolyte NPs were synthesized using liquid-feed flame spray pyrolysis, then processed to pellets (0.5 mm thick) and thin (\leq 50 μ m) films. $Mg_{0.5}Ce_{0.2}Zr_{1.8}(PO_4)_3$ electrolytes including pellets and films after sintering at 1200 °C offer densities and optimized phase purities thereby offering the highest ionic conductivities among the $Mg_{0.5}Ce_xZr_{2-x}(PO_4)_3~(x=0.1,~0.2~and~0.3)$ compositions in this preliminary work. MZPCe_{0.2} pellets show ionic conductivities of $3.8 \times 10^{-4}\,mS\,cm^{-1}$ at 200 °C, while thin (ca. 45 μ m thick) films offer values of $1.9 \times 10^{-4}\,mS\,cm^{-1}$ under the same conditions likely due

Chemical compositions	T (°C)	$\sigma_t (mS cm^{-1})$	Processing methods	Shapes	Refs.
MZPCe _{0.2}	25	$2.0 imes 10^{-7}$	LF-FSP/TC/S	Films/45 \pm 5 μ m thick	this work
	200	$1.9 imes 10^{-4}$			
	280	$3.1 imes 10^{-3}$			
	500 [†]	$1.9 imes 10^{-1}$			
	800 [†]	3.65			
MZPCe _{0.2}	25	2.6×10^{-6}	LF-FSP/CIP/S	Pellets/0.5 mm thick	this work
	200	$3.8 imes 10^{-4}$			
$Mg_{0.5}Zr_2(PO_4)_3$	25	$1.0 imes 10^{-3}$	SG/C/S	Pellets	[15]
	500	$7.1 imes 10^{-2}$			
$Mg_{0.5}Zr_2(PO_4)_3$	400	$2.9 imes 10^{-2}$	G/C/HP	Pellets/1–2 mm thick	[29]
	800	$6.1 imes 10^{-1}$			
$Mg_{0.5}Zr_2(PO_4)_3$	800	$6.9 imes10^{-1}$	SG/C/S	Pellets	[17]
Mg _{1.4} Zr ₄ P ₆ O _{24.4} +0.4Zr ₂ O(PO ₄) ₂	800	2.9	G/C/S	Pellets	[23]
$Mg_{0.9}(Zr_{0.6}Fe_{0.4})_2(PO_4)_3$	25	$1.3 imes 10^{-2}$	SG/C/S	Pellets	[16]
	500	$7.2 imes 10^{-2}$			
$Mg_{0.5}Si_2(PO_4)_3$	25	$1.8 imes 10^{-2}$	SG/C/S	Pellets	[27]
$(Mg_{0.1}Hf_{0.9})_{4/3.8}Nb(PO_4)_3$	300	2.1×10^{-3}	CP/C/S	Pellets	[18]

Note: TC—tape casting, S-sintering at atmospheric pressure, CIP—cold isostatic pressing, SG—sol-gel, C—calcination, G—grinding mixed powders in a mortar, HP—hot pressing, CP—co-precipitation.

to the imperfect surface finishes and possible surface impurities. Note that Ce free compositions do not sinter to full density under the conditions used here indicating the advantage to doping with Ce.

Arrhenius based estimates for ionic conductivities at 400 °C suggest values near or superior to $10^{-2} \,\mathrm{mS} \,\mathrm{cm}^{-1}$ in keeping with the best values reported in the literature. The important contribution here is the significant reduction in thickness in these thin film electrolytes compared to pellets which offer IASR values of $1400 \,\Omega \,\mathrm{cm}^2$ at $\approx 300 \,^{\circ}$ C and are estimated to offer IASR values of $110 \,\Omega \,\mathrm{cm}^2$ at 400 °C providing the potential for high energy density solid-state batteries. Thin film electrolytes are therefore promising for development of high-performance all-solid-state Mg-ion batteries operated at medium temperatures.

The optimization of the electrolyte composition, microstructure, and processing conditions is underway which is expected to achieve maximum ionic conductivities to open a new door for the applications of rechargeable batteries. Substantial research efforts will be made to develop competitive magnesium electrolytes by processing of thin films with new chemical compositions.

The results reported here suggest that it may be possible to greatly improve the Mg^{2+} conductivities in dense, thin ceramic electrolytes to the point where the operational temperatures of solid state batteries made from them will function at temperatures below 200 °C and perhaps eventually below 100 °C, as we have successfully shown recently for dense, flexible Li⁺ ceramic electrolytes [37–39].

Conflicts of interest

There are no conflicts to declare.

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Appendix A. Supplementary data

Supplementary data related to this article can be found at https://doi.org/10.1016/j.electacta.2018.04.015.

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